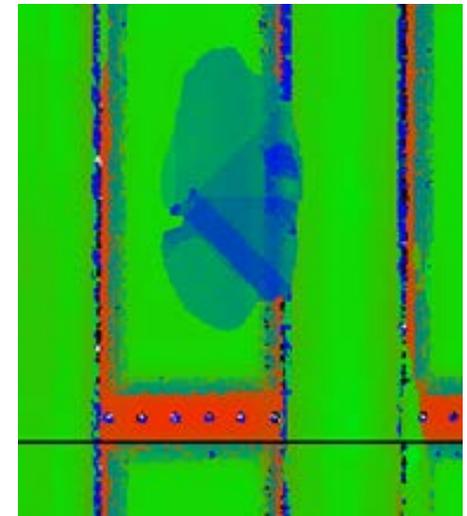
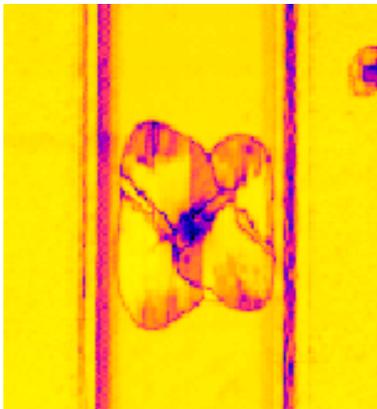
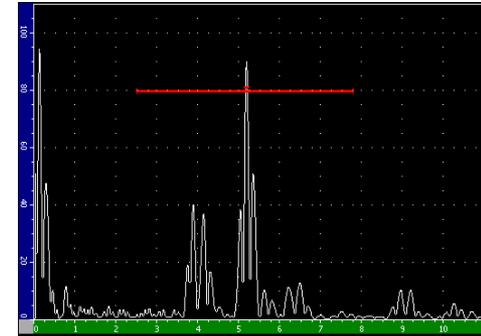
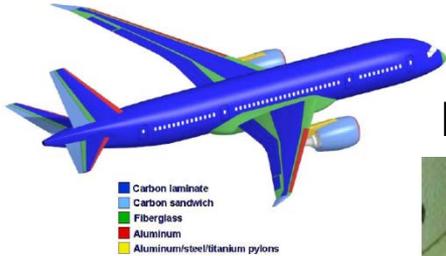


Inspection Methods for Characterizing Subsurface Impact Damage in Solid Laminate Aerospace Composites

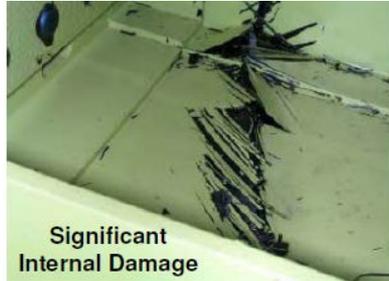


**Stephen Neidigk, Dennis Roach,
Tom Rice, Randy Duvall
FAA Airworthiness Assurance Center
Sandia National Labs**

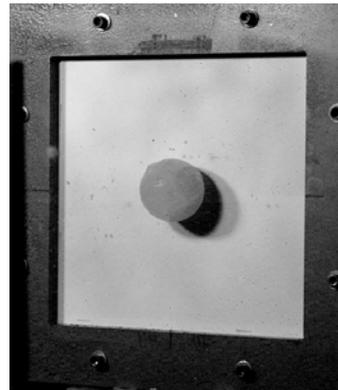
Presentation Outline



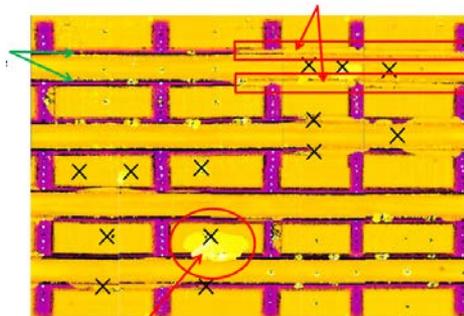
Introduction and Background



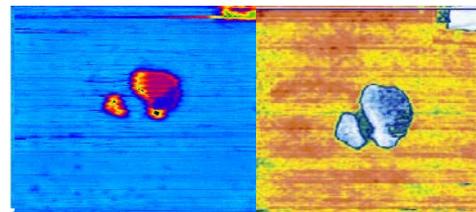
Motivation



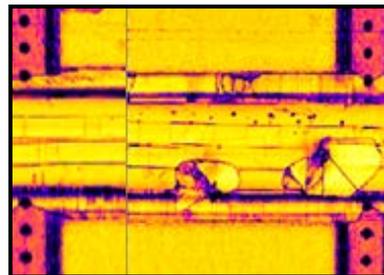
Ice Impact Damage on Laminate Plates



Conclusions



Side-by-Side Inspection Comparison of NDI Techniques



Full-Scale Panel Impact Testing

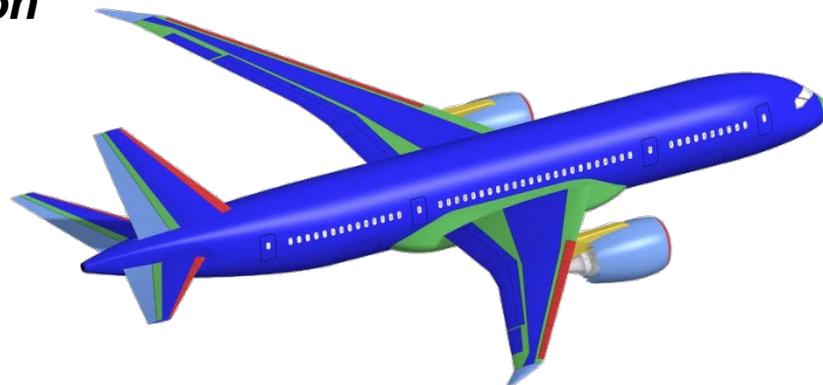
- Simulated Hail
- Blunt
- Hardened



Program Motivation - Extensive/increasing use of composites on commercial aircraft and increasing use of NDI to inspect them

Composite Structures on Boeing 787 Aircraft

- Carbon laminate
- Carbon sandwich
- Fiberglass
- Aluminum
- Aluminum/steel/titanium pylons



Composite Center Wing Box



A380 Pressure Bulkhead

Program Goals: Assess & Improve Flaw Detection Performance in Composite Aircraft Structure

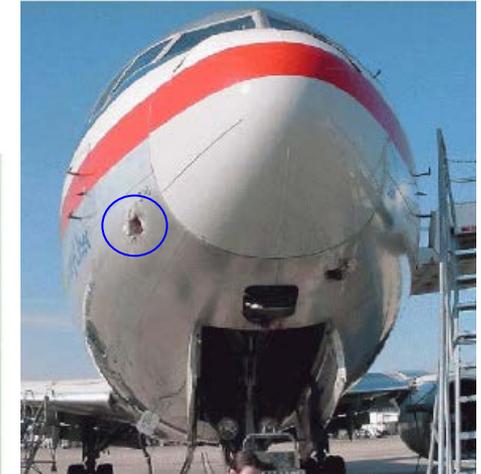


Sources of Damage in Composite Structure



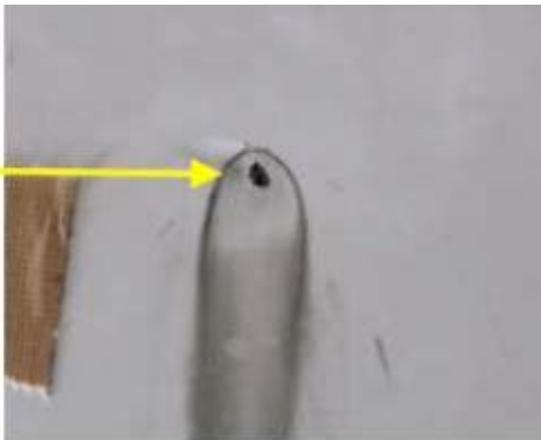
Lightning Strike on Thrust Reverser

Ground Support Equipment Impact



Bird Strike

Lightning Strike on Fuselage



Towing Damage

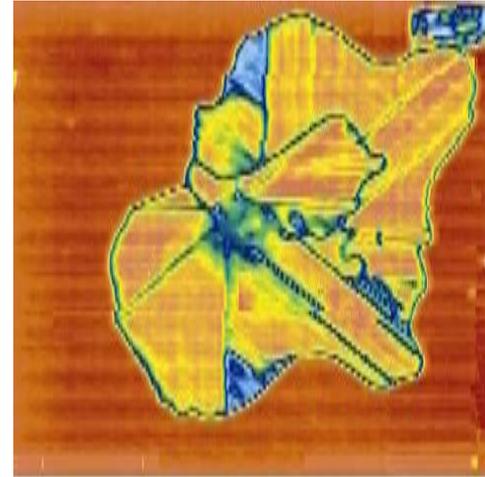
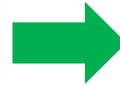


Inspection Challenge – Hidden Impact Damage

Internal delamination from ice impact

Extent of visible damage

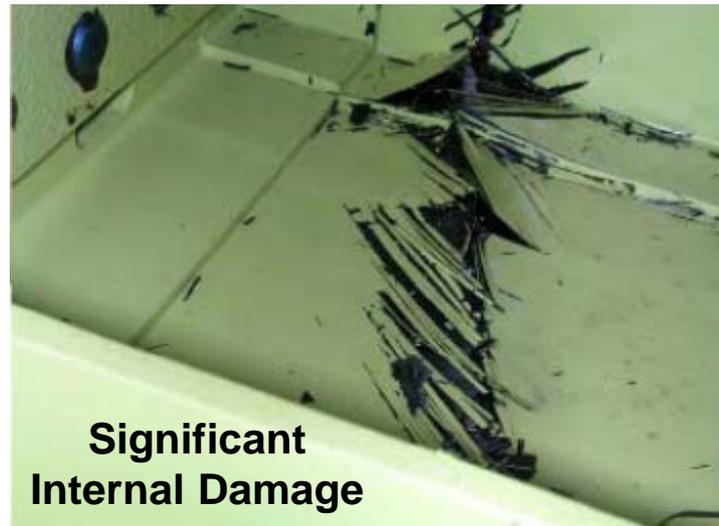
44 in² Delamination



Damage from ground vehicle



Extent of Visible
Damage from Outside



Significant
Internal Damage



AANC Composite Programs

- Industry wide NDI Reference Standards
- NDI Assessment: Honeycomb Structures
- NDI Assessment: Solid Laminate Structures
- Composite Heat, UV, and Fluid Ingress Damage
- Composite Repairs and Porosity
- Composite NDI Training and NDI Proficiency Specimens



*Inspection
Task Group*

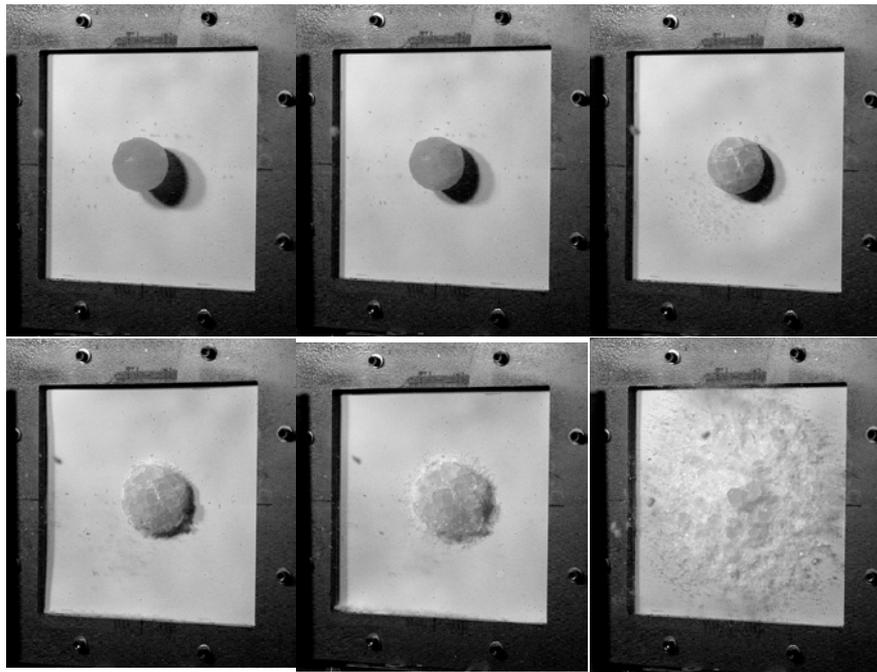
Composite Impact Study

Multiple **impact parameters** must be studied – hardness of impactor, low mass-high velocity impact, high mass-low velocity impact, angle of impact, surface demarcations & visual clues, panel stiffness

- Identify which impact scenarios are of major concern to aircraft maintenance
- Identify key parameters governing impact damage formation
- Relate damage threat & structural integrity to capabilities of NDI to detect hidden impact damage in laminates
- Develop methodology for impact threat characterization



Ice Impact Testing at UCSD

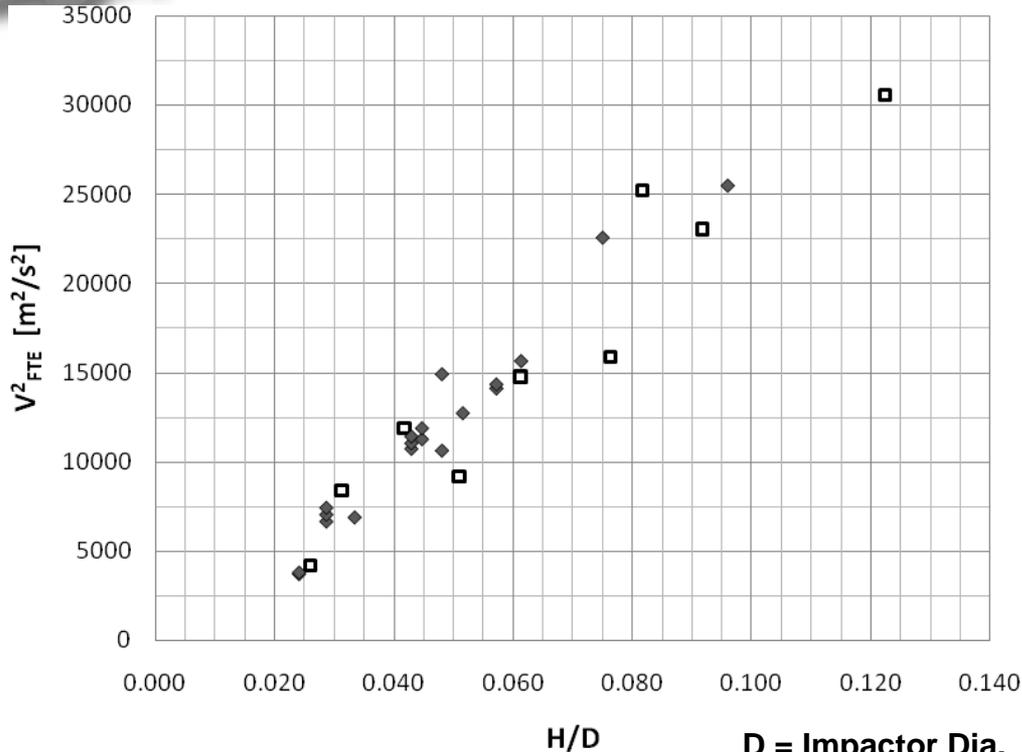


UCSD High Velocity Gas Gun

**Still Images from 61 mm Ice Impact
on 8 Ply Carbon Panel at 72 m/s**

Joint Effort: UCSD (Prof. Hyonny Kim)

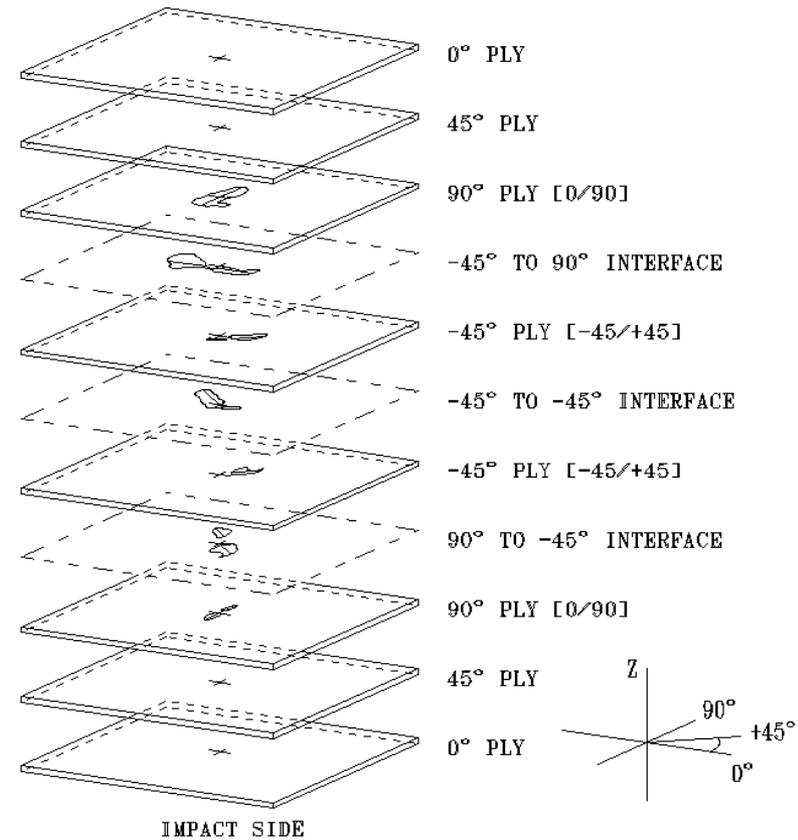
Damage in Composite Laminates from Ice Impact



□ T800/3900-2 Tape (Current Data)

◆ AS4/977 and AS4/8552 Fabric (Kim et al. 2003)

Failure Threshold (Energy) Velocity



Impact-Induced Damage Morphology for 8 Ply Panel; 42.7 mm Ice at 120.4 m/s (267 J)

Selected panels were sectioned and observed by microscopy to map out the damage. The laminates develop the series of classic peanut shaped delaminations/fractures that stack together to give the overall appearance shown in the scans



Composite Impact Study – Hail Impact Task Description

- 112 carbon composite panels were fabricated using BMS8-276N uniaxial material; consisted of 8, 16, and 24 ply configurations (12” x 12”)
- All panels were impacted with ice balls of different diameters and velocities to simulate hail and create various levels of impact damage
- The goal was to create damage associated with Failure Threshold ~ BVID range & complete NDI to evaluate the sensitivity of each method in detecting and sizing the damaged area (reliable, sensitive, gate deployment, cost effective)
- NDI methods used for this evaluation include: Through Transmission Ultrasonics (TTU), Phased Array UT, Pulse-Echo UT, Resonance, Flash Thermography, Damage Checker (PE-UT), Mechanical Impedance Analysis, Low Frequency Bond Test



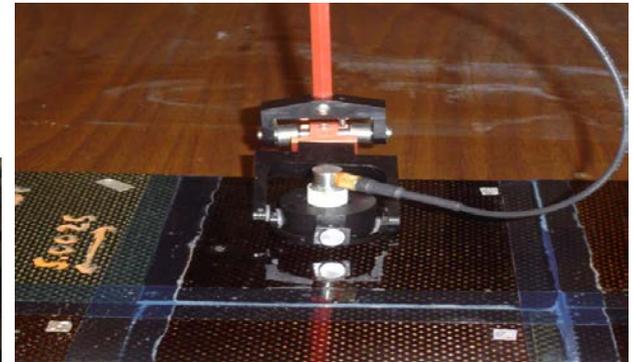
Composite Impact Damage – Inspection Methods Deployed



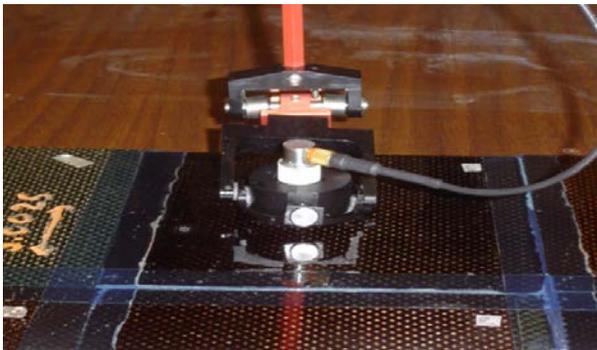
TTU



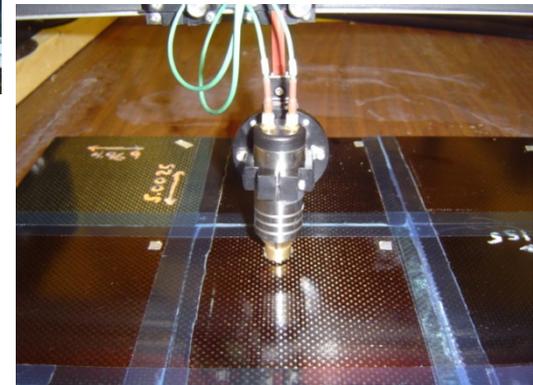
Thermography



MAUS PE



**MAUS
Resonance**



MAUS MIA

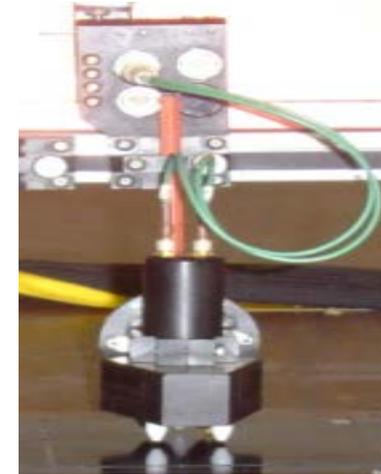
Composite Impact Damage – Inspection Methods Deployed



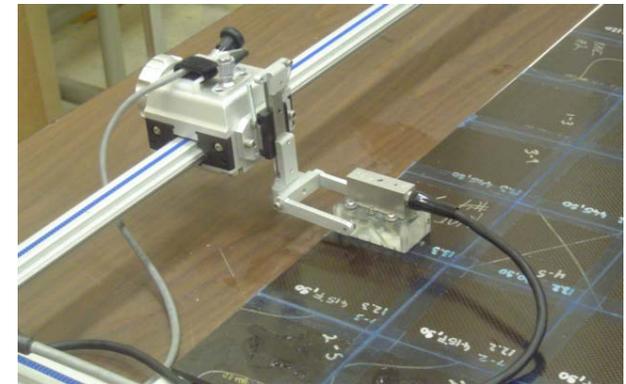
**Damage Check Device
(Pulse-Echo UT)**



**V-95
(Mechanical Impedance
Analysis)**



MAUS LFBT



Omniscan Phased Array UT

TC-16-25

Impact Energy (J) - 525.1

Example Result

Flaw Size MAUS PE (mm²) - 37,128

Impact Velocity (m/s) - 212.44

Flaw Size Omniscan PE (mm²) - 28,380

Projectile Size (mm) - 38.1

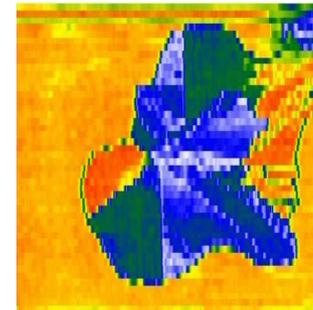
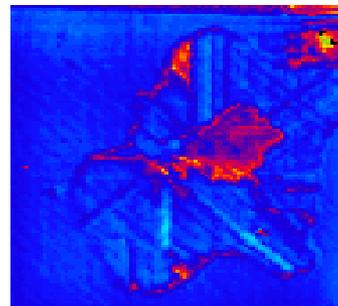
Flaw Size TTU UCSD (mm²) - 26439

Picture

TTU

MAUS PE

Omni PE

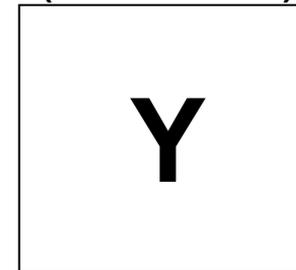
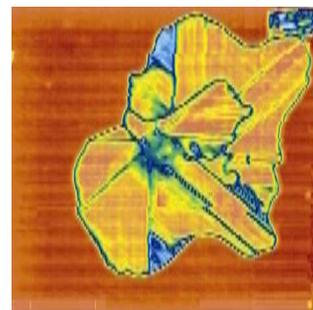
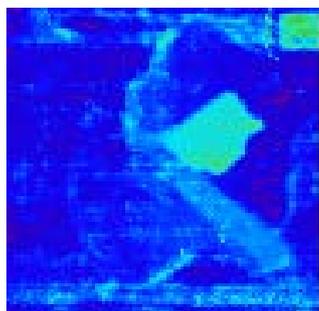
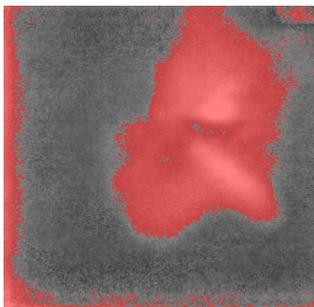


IR

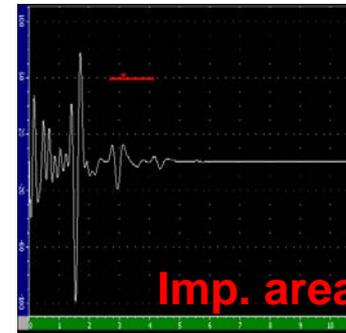
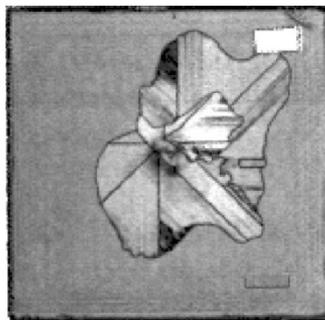
MAUS Resonance

Omni PA

Ramp Damage Checker
(flaw indicated)



Laser UT



TC-24-19

Impact Energy (J) - 1,268.1

Example Result

Flaw Size MAUS PE (mm²) - 9,413

Impact Velocity (m/s) - 153.46

Flaw Size Omniscan PE (mm²) - 9,439

Projectile Size (mm) - 61

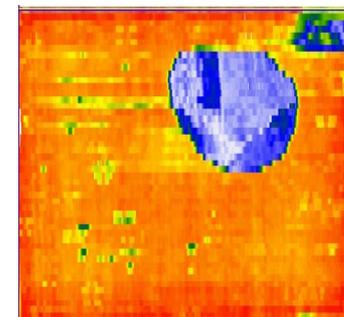
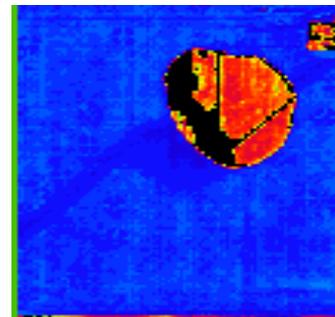
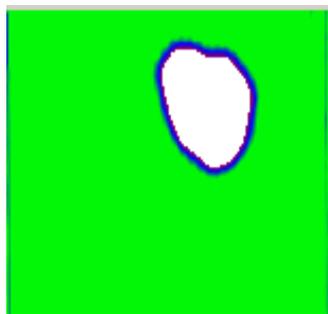
Flaw Size TTU UCSD (mm²) - 8,022

Picture

TTU

MAUS PE

Omni PE

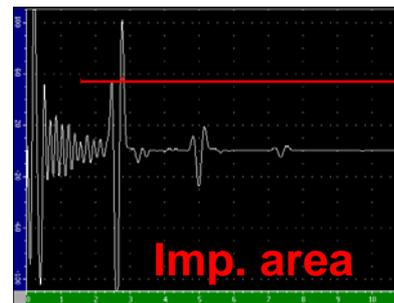
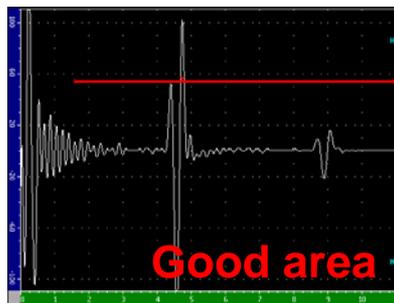
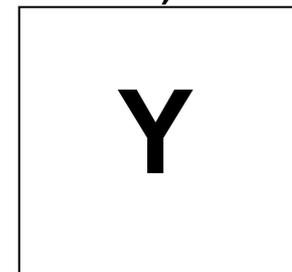
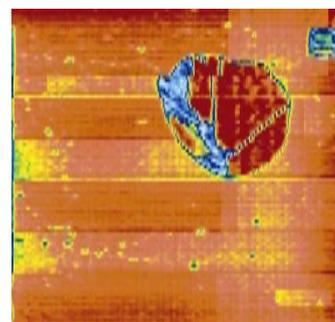
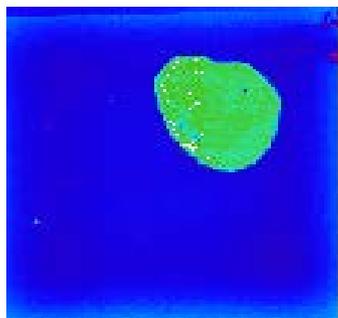
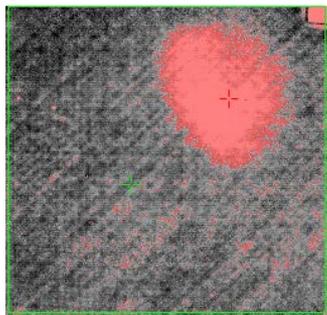


IR

MAUS Resonance

Omni PA

Ramp Damage Checker
(flaw indicated)



FAA William J. Hughes
Technical Center



TC-08-29

Impact Energy (J) - 306.7

Example Result

Flaw Size MAUS PE (mm²) - 703

Impact Velocity (m/s) - 99

Flaw Size Omniscan PE (mm²) - 554

Projectile Size (mm) - 50.8

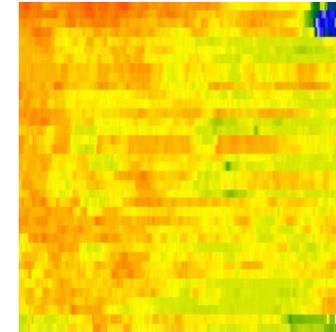
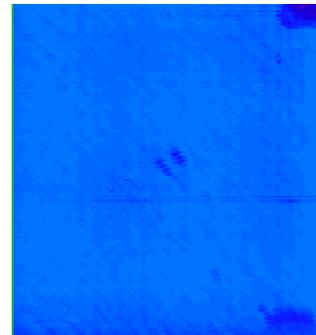
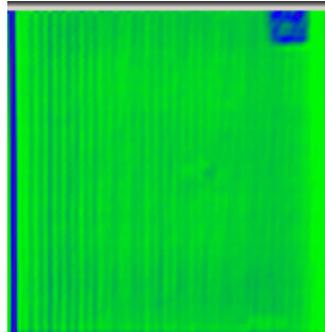
Flaw Size TTU UCSD (mm²) - 0

MAUS PE

Omni PE

Picture

TTU

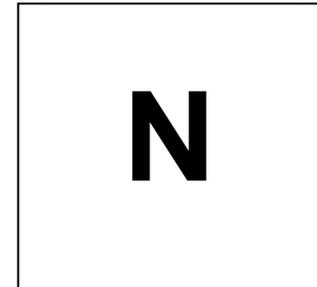
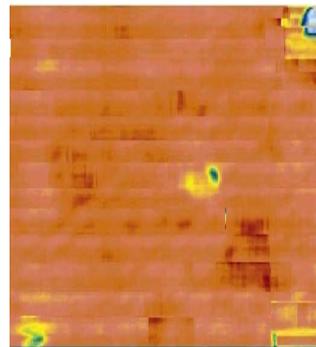
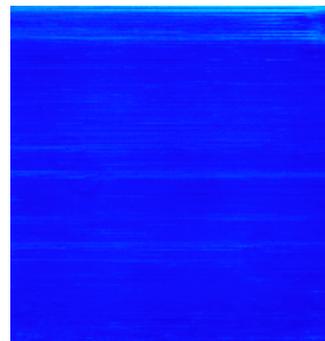
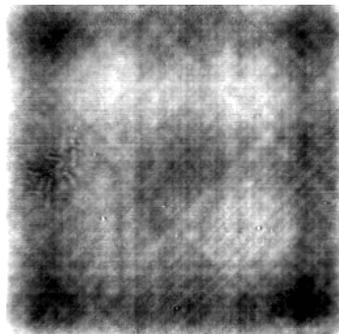


IR

MAUS Resonance

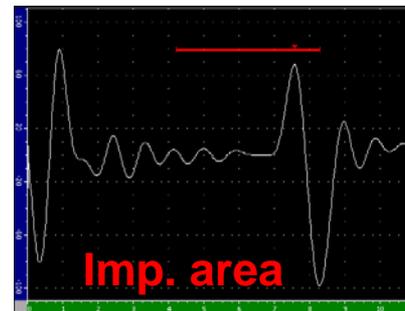
Omni PA

**Ramp Damage Checker
(flaw indicated)**



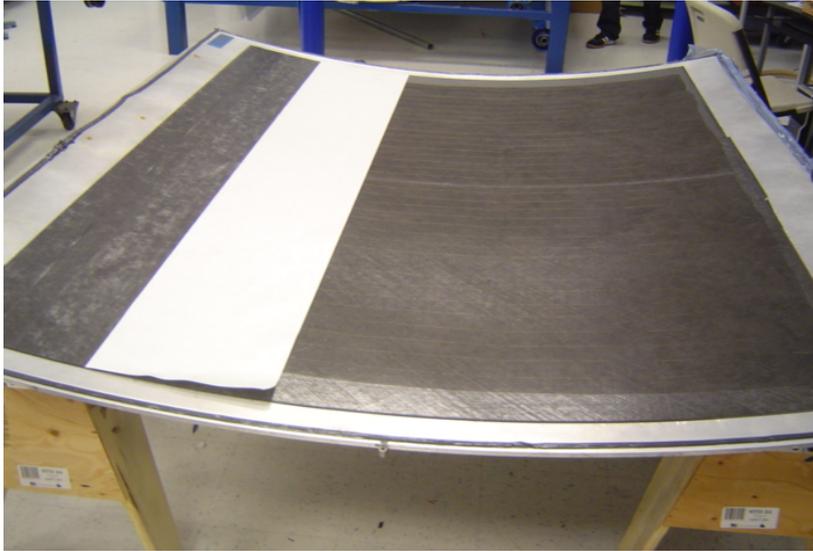
A-scan Ref

FAA William J. Hughes
Technical Center

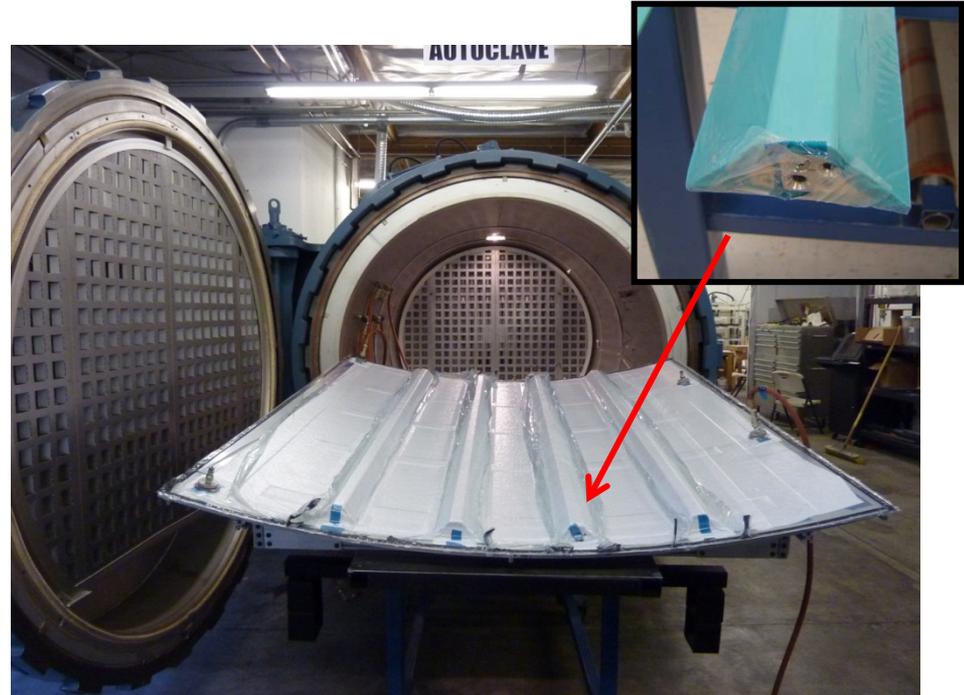


Full-Scale Fuselage Test Panel Fabrication

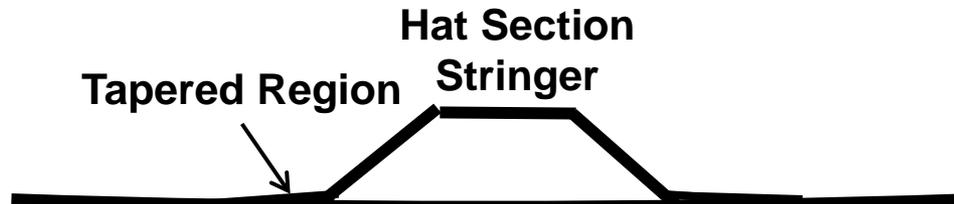
Not flat, simple structures



Skin - Curved Construction



Autoclave Cured (350° F at 90 psi)

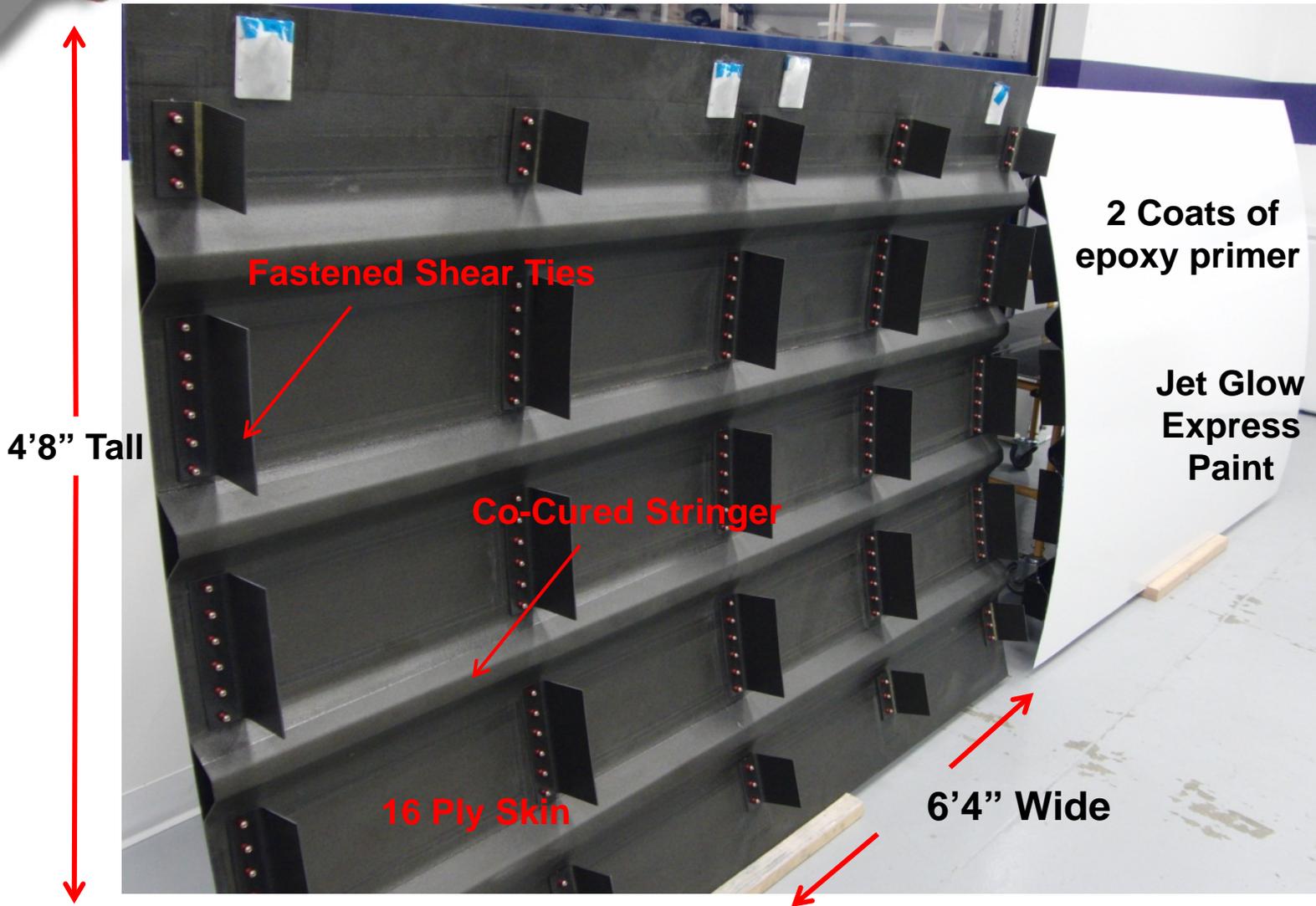


Quasi-Isotropic Lay Up $[0,+45,90,-45]_{2(s)}$

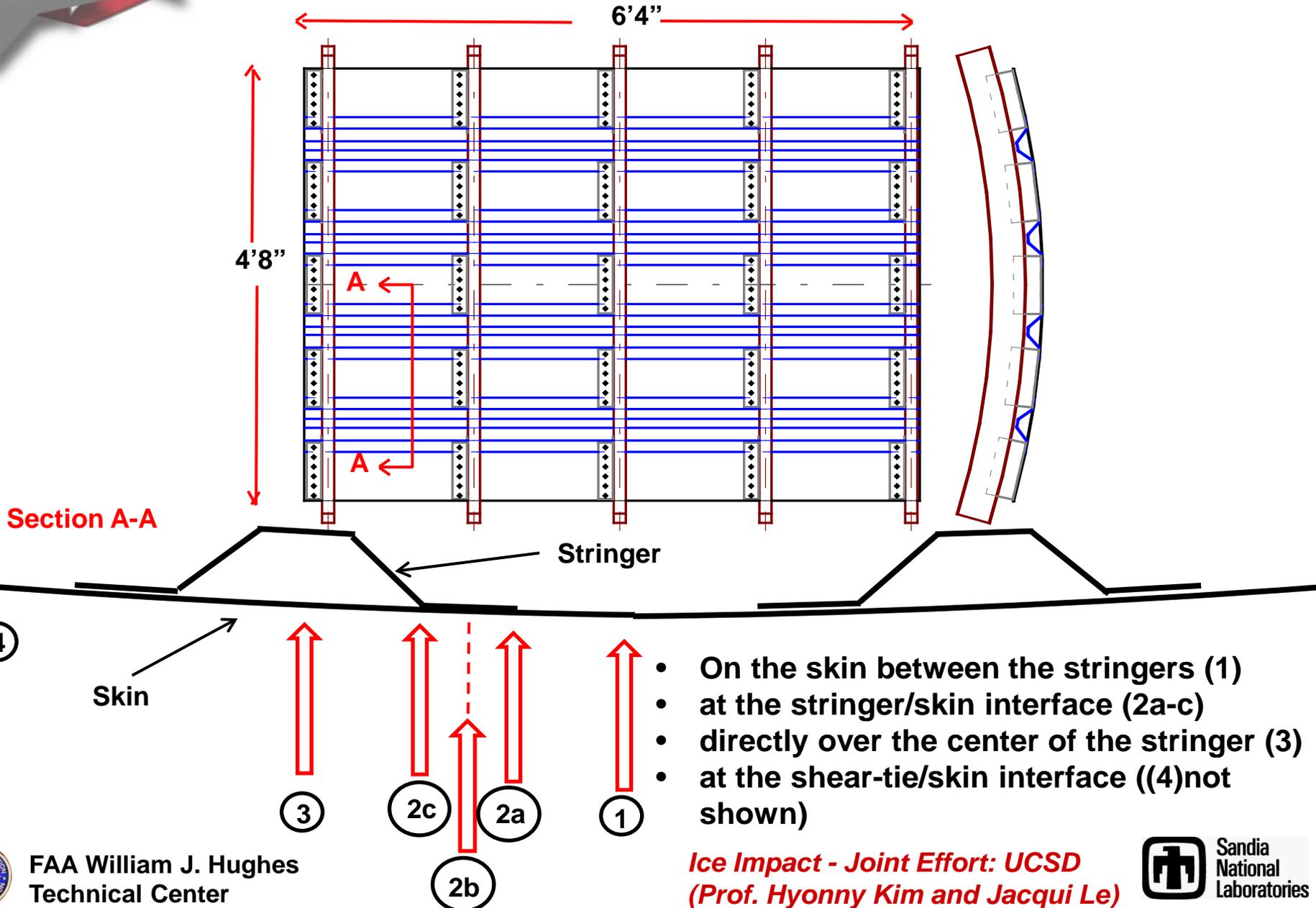
T800 unidirectional pre-preg tape with a 3900 series resin system (BMS8- 276)



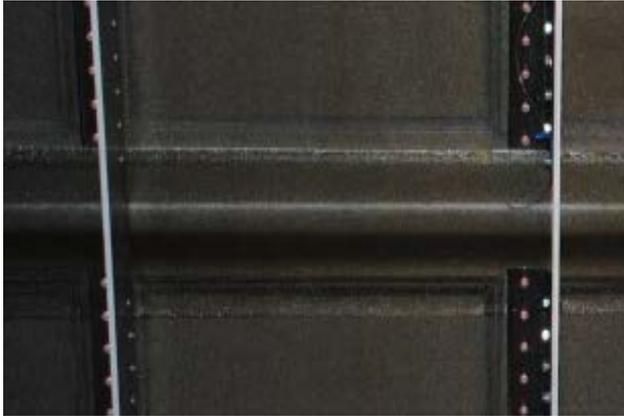
Full-Scale Fuselage Test Panels



Impact Locations of Interest

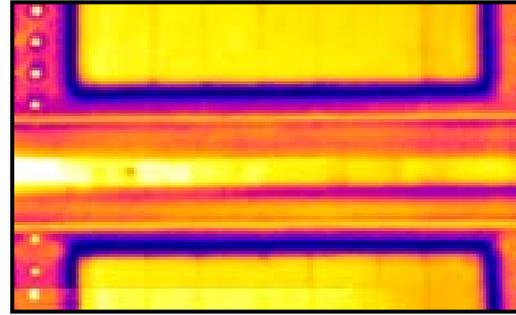


C-Scan Inspection Interpretation

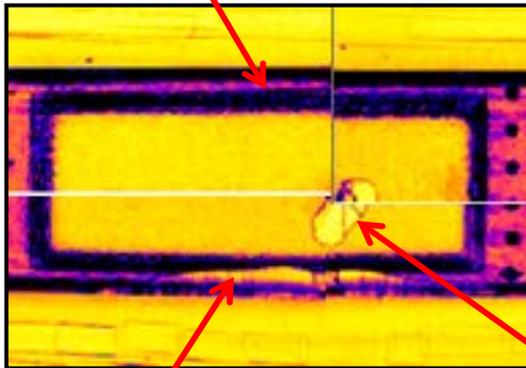


Fully bonded stringer flange

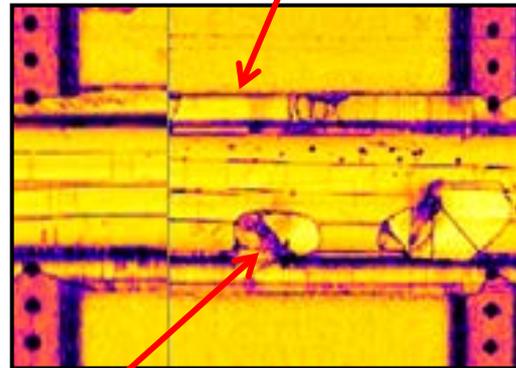
Pristine Area



Fully disbonded stringer flange



Partially delaminated stringer flange



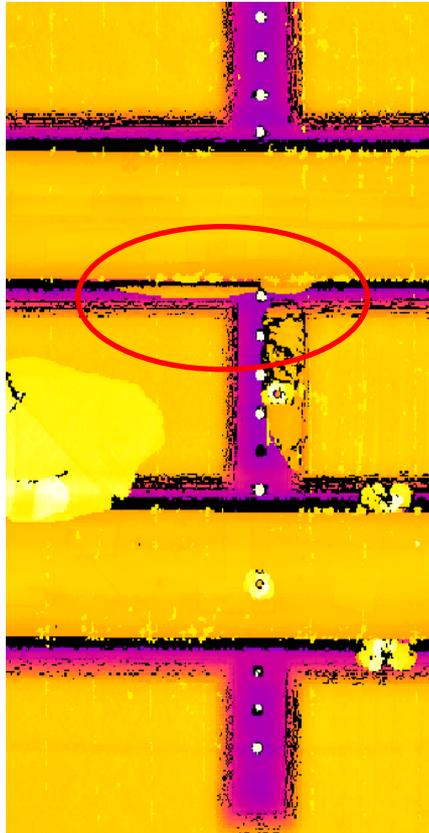
Interply delamination in the skin



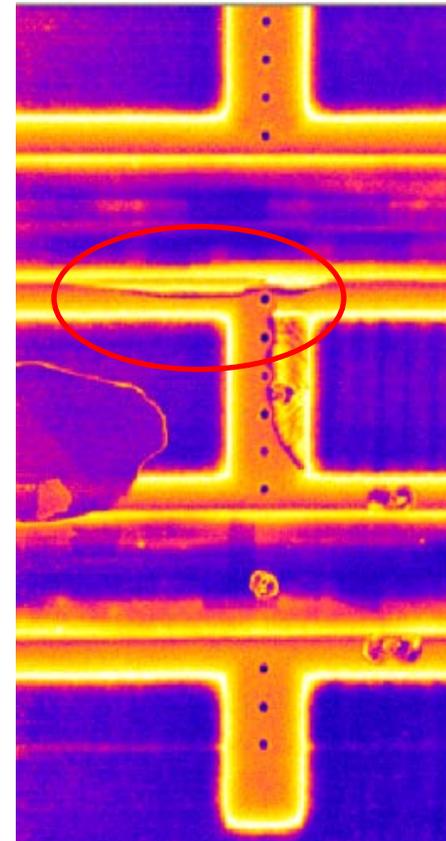
Comparison of NDI Techniques



UT Amplitude



UT Time of Flight



UT Resonance

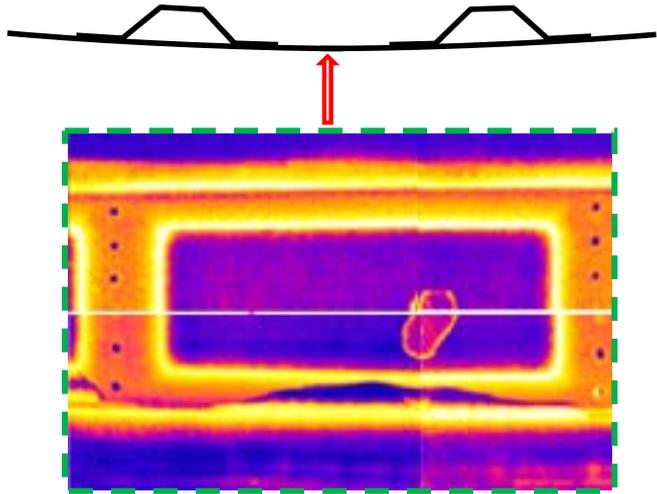
TOF and Resonance enhance detection of small disbonds



Ice Impact Testing Results

2.4 in diameter simulated hail impact tests were conducted between 50 and 120 m/s.

Mid-Bay Impacts

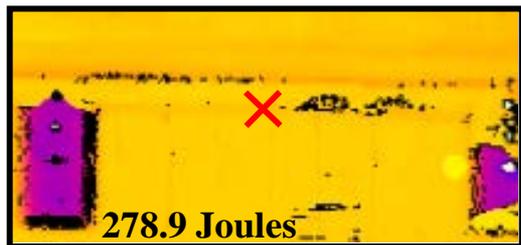


UT Resonance Y-Plot

Terminal velocity ~ 30 to 35 m/s)

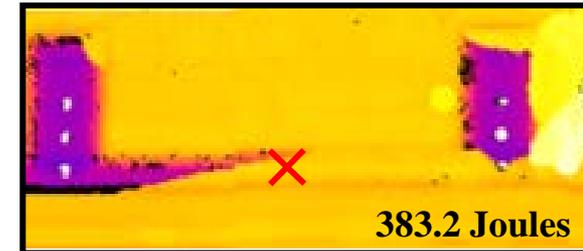
- Induce both interply delamination and substructure disbonding
- No damage was visually detectable from the surface
- Damage was initiated at approximately 230 Joules (~67 m/s)

Stringer Flange Impacts



(0.0) / (23.16)

- Induce only substructure flange disbonding
- No damage was visually detectable from the surface
- Damage was initiated at approximately 170 Joules (~56 m/s)

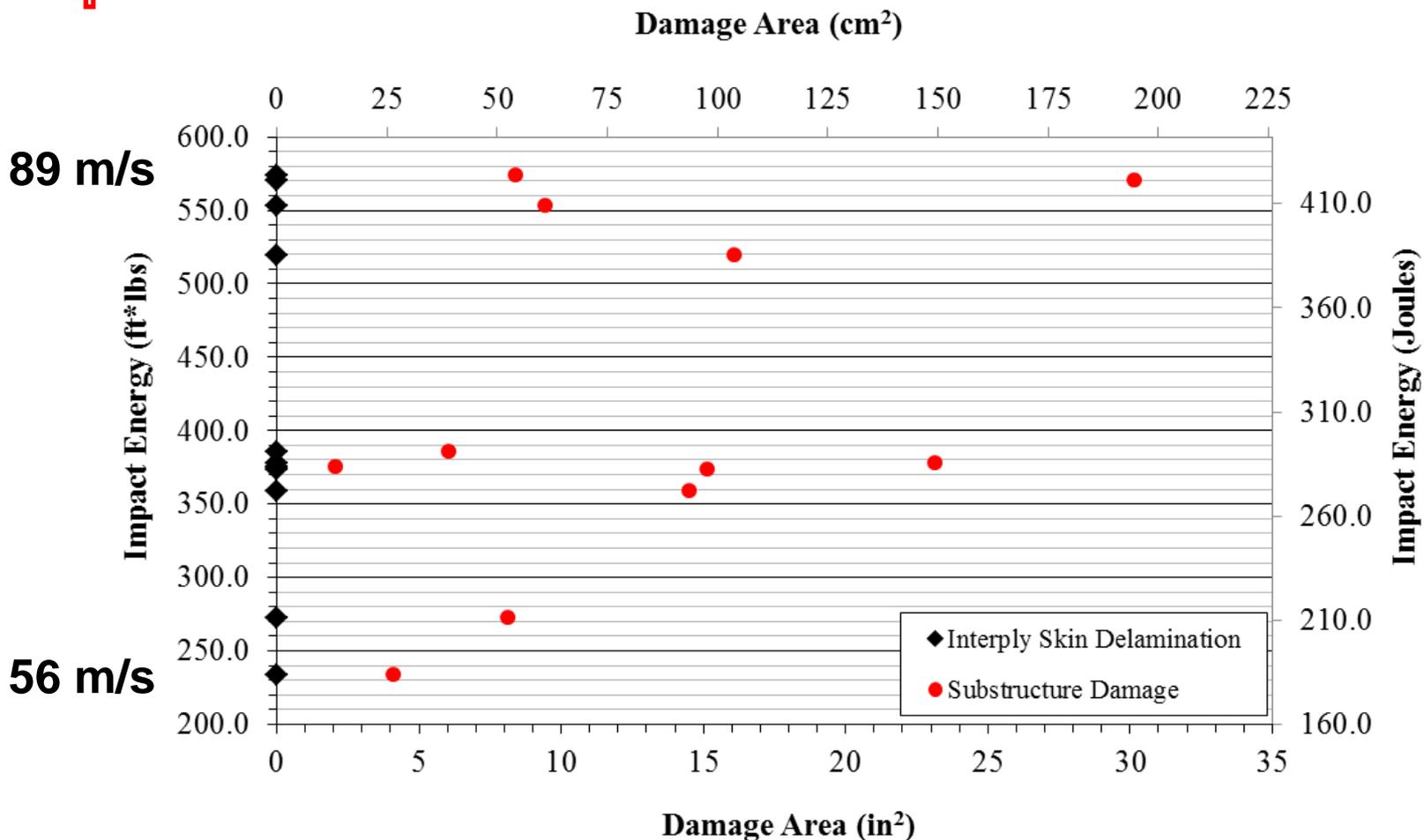


(0.0) / (16.09)



Ice Impact Testing Results

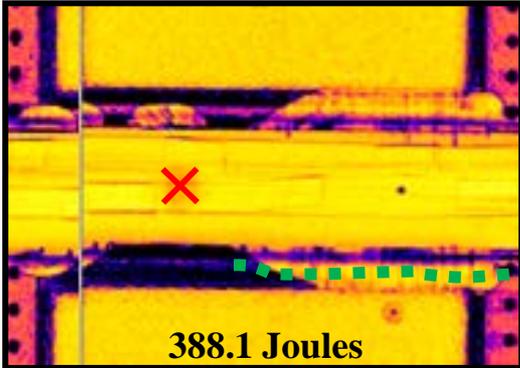
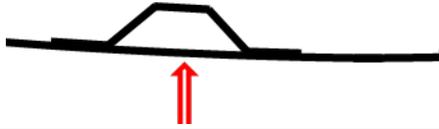
Stringer Flange Impacts



Initiated substructure disbonding only, no interply delamination detected with these impacts



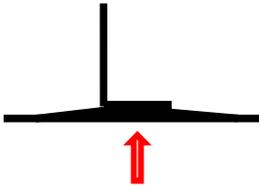
Mid-Stringer Impacts



Ice Impact Testing Results

- Induce both interply delamination and substructure disbonding (mostly flange disbonding)
- No damage was visually detectable from the surface
- Possible to initiate damage at less than 400 Joules

Shear Tie Impacts



- Induce built-up pad section delamination and cracked shear ties
- Damage was visually detectable from the surface (cracks, surface markings at approximately 700 Joules (115 m/s))



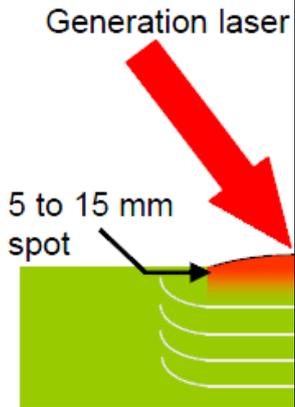
All shear tie impacts cracked the impacted shear tie



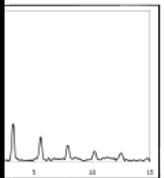
iPhoton Solutions Full Panel Inspection Results



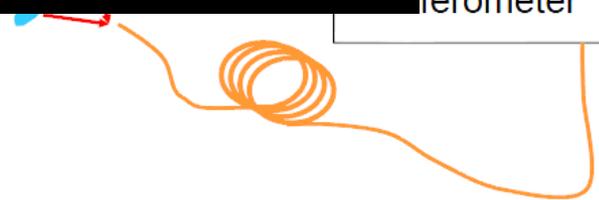
- Laser-ultra
- Conventional
- High speed
- Uses comm



ected
and



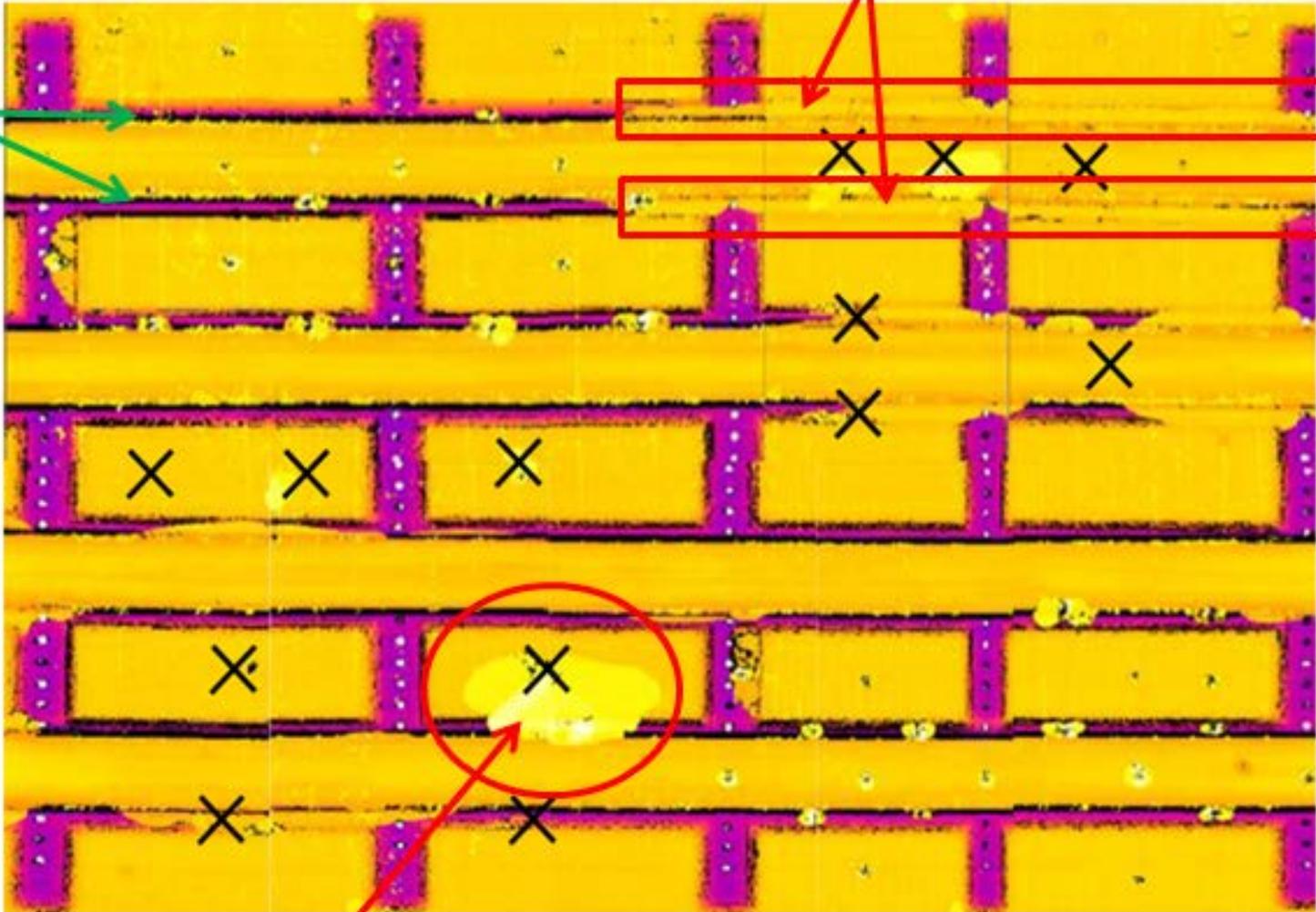
ferometer



Significant Damage with No Visual Indication

40 inch stringer disbond

Co-cured stringer



54 in² Interply delamination

Conclusion

•AANC Composite Impact Studies Include:

- Identifying impact scenarios of concern
- Identifying key parameters governing impact damage
- Characterizing impact damage below the BVID level
- Relating damage threat to capabilities of NDI

•**NDI ability** to detect impact damage was assessed in FTE ~ BVID range → sensitivity, sizing, procedures, deployment

The presented work shows that...

- This structure is robust against hail impact
- Large damage can occur with no surface visual indication
- Impacts can initiate substructure damage away from the impact site
- Substructure impacts induce damage at less energy than mid-bay impacts
- Hard tip impacts induce localized, near surface damage that are typically visibly detectable from the surface (depends on tip diameter and hardness)

Ongoing efforts...

- Subsurface damage can be difficult to detect with conventional NDI (ref. AANC SLE POD)
- Characterized panels are being used to assess emerging NDI technologies





Sponsors and Collaborators

Thanks to our sponsors and collaborators

- **Dave Westlund – FAA TC**
- **Rusty Jones – FAA**

- **Professor Hyonny Kim – UC San Diego**
- **Jacqui Lee – UC San Diego**

